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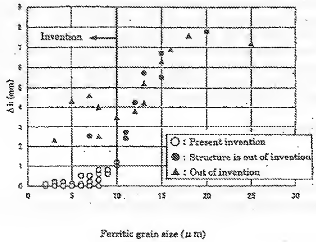
(54) HOT DIP ZINC PLATED STEEL SHEET HAVING HIGH STRENGTH AND METHOD FOR PRODUCING THE SAME

(57) The invention relates to a high strength hot-dip galvanized steel sheet consisting essentially of 0.03 to 0.25% C, 0.7% or less Si, 1.4 to 3.5% Mn, 0.05% or less P, 0.01% or less S, 0.05 to 1% Cr, 0.005 to 0.1% Nb, by mass, and balance of Fe, and being made of a composite structure of ferrite and secondary phase, and having an average grain size of the composite structure of 10 μm or smaller. Since the high strength hot-dip galvanized steel sheet of the present invention hardly induces softening at HAZ during welding, it is applicable to structural members of automobiles for "Tailor Welded Blanks" (TWB).

FIG. 1



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Description

TECHNICAL FIELD

[0001] The present invention relates to a high strength hot-dip galvanized steel sheet having tensile strength above 700 MPa, and particularly to a high strength hot-dip galvanized steel sheet that hardly induces softening at heat-affected zone (HAZ) during welding and that has excellent formability, and a method for manufacturing thereof.

BACKGROUND ART

[0002] High strength hot-dip galvanized steel sheets having higher than 440 MPa of tensile strength are used in wide fields including construction materials, machine and structural members, and structural members of automobiles owing to the excellent corrosion resistance and the high strength.

[0003] Responding to ever-increasing severity of requirements on formability in recent years, various technologies to improve the formability of that type of high strength hot-dip galvanized steel sheet have been introduced. For example, according to JP-A-5-311244, (the term "JP-A" referred herein signifies the "unexamined Japanese patent publication"), a Si-Mn-P bearing hot-rolled steel sheet is heated to temperatures at or above Ac1 transformation point in a continuous hot-dip galvanizing line, and the heated steel sheet is quenched to Ms point or below to generate martensite over the whole or in a part thereof, then the martensite is tempered using the heat of the hot-dip galvanizing bath and of the alloying furnace. According to JP-A-7-54051, a hot-rolled steel sheet of Mn-P-Nb(-Ti) bearing is coiled at a low temperature after hot-rolled, which steel sheet is then subjected to hot-dip galvanizing to let pearlites or cementites disperse finely in the fine ferrite matrix to improve the stretch flangeability.

[0004] On the other hand, structural members of automobiles have recently been adopting steel sheets of different strength or different thickness which are joined together by laser welding or mush-seam welding, called "Tailor Welded Blanks" (TWB). Thus, the characteristics of welded part are also emphasized.

[0005] The high strength hot-dip galvanized steel sheet manufactured by the method disclosed in JP-A-5-311244 aiming at the improvement of formability of the steel sheet itself, however, is not applicable to the structural members of automobiles or the like because the softening at HAZ likely occurs during welding to induce degradation of formability and strength at the welded part. It is because, though the mechanism of strengthening is based on the second phase obtained by rapid-cooling austenite, the ferrite and the second phase are not fully homogeneously refined. The term "second phase" referred herein signifies a phase consisting of at least one structure selected from the group consisting of martensite and bainite. The high strength hot-dip galvanized steel sheet manufactured by the method disclosed in JP-A-7-54051 is difficult to stably have tensile strength exceeding 700 MPa, particularly above 780 MPa, because the structure thereof is a ferrite matrix with finely dispersed pearlites or cementites.

DISCLOSURE OF THE INVENTION

[0006] An object of the present invention is to provide a high strength hot-dip galvanized steel sheet that hardly induces softening at HAZ during welding, that has tensile strengths above 700 MPa, and that assures excellent formability, and a method for manufacturing thereof.

[0007] The object is attained by a high strength hot-dip galvanized steel sheet which consists essentially of 0.03 to 0.25% C, 0.7% or less Si, 1.4 to 3.5% Mn, 0.05% or less P, 0.01% or less S, 0.05 to 1% Cr, 0.005 to 0.1% Nb, by mass, and balance of Fe, and is made of a composite structure of ferrite and secondary phase, further has an average grain size of the composite structure of 10 μm or smaller.

[0008] The high strength hot-dip galvanized steel sheet can be manufactured by the method containing the steps of: hot-rolling a steel slab consisting essentially of 0.03 to 0.25% C, 0.7% or less Si, 1.4 to 3.5% Mn, 0.05% or less P, 0.01% or less S, 0.05 to 1% Cr, 0.005 to 0.1% Nb, by mass, and balance of Fe, at temperatures of Ar3 transformation point or above; cooling the hot-rolled steel sheet within a temperature range of 800°C to 700°C at a cooling rate of 5°C/sec or more, followed by coiling the cooled steel sheet at temperatures of 450°C to 700°C; and galvanizing the steel sheet after heating the steel sheet to a temperature range of 760°C to 880°C, and by cooling the steel sheet to temperatures of 600°C or below at a cooling rate of 1°C/sec or more in a continuous hot-dip galvanizing line.

BRIEF DESCRIPTION OF THE DRAWINGS

[0009]

Fig. 1 is a graph showing the relation between Δh and average grain size of ferrite.

Fig. 2A and Fig. 2B are graphs showing the hardness profile on a laser-welded cross section of steel sheet of an

example according to the present invention and a comparative example, respectively.

EMBODIMENTS OF THE INVENTION

[0010] The inventors of the present invention studied the characteristics of high strength hot-dip galvanized steel sheets after welded, and found that the softening at HAZ during welding could be prevented and that excellent formability could be attained by adding Nb and Cr to the steel and by establishing a composite structure of ferrite and second phase, which composite structure has 10 µm or smaller average grain size. Owing to the presence of the hard second phase of martensite or bainite, giving high dislocation density, to the strengthening of secondary precipitation caused by Cr, and to the effect of suppressing recovery of dislocation caused by the fine NbC precipitation, the softening at HAZ could be prevented, and, further with the refinement of structure, the excellent formability could be attained. The detail description is given below.

1) Steel compositions

[0011] The high strength hot-dip galvanized steel sheet according to the present invention consists essentially of the elements described below and balance of Fe.

C

[0012] Carbon is an essential element to attain high strength. To obtain tensile strengths above 700 MPa, the C content of 0.03% or more is necessary. If, however, the C content exceeds 0.25%, the volumetric percentage of the second phase increases to induce binding of grains to each other thus to increase the grain size, which induces softening at HAZ during welding and degrades the formability. Therefore, the C content is specified to a range of from 0.03 to 0.25%.

Si

[0013] Silicon is an effective element for stably attaining a ferrite + martensite dual phase structure. If, however, the Si content exceeds 0.7%, the adhesiveness of zinc coating and the surface appearance significantly degrade. Accordingly, the Si content is specified to 0.7% or less.

Mn

[0014] Manganese is an essential element for attaining high strength, similar with C. To obtain 700 MPa or higher tensile strength, at least 1.4% of the Mn content is required. If, however, the Mn content exceeds 3.5%, the grain size of the second phase increases to induce softening at HAZ during welding and to degrade the formability. Consequently, the Mn content is specified to a range of from 1.4 to 3.5%.

P

[0015] Phosphorus is an effective element for stably attaining a ferrite + martensite dual phase structure, similar with Si. If, however, the P content exceeds 0.05%, the toughness at the welded part degrades. Therefore, the P content is specified to 0.05% or less.

S

[0016] Since S is an impurity, smaller amount is more preferable. If the S content exceeds 0.01%, the toughness at the welded part significantly degrades, similar with P. Consequently, the S content is specified to 0.01% or less.

sol.Al

[0017] Although sol.Al is an effective element as deoxidizing element, over 0.10% of sol.Al content gives degraded formability. Accordingly, the sol.Al content is preferably 0.10% or less.

N

[0018] If N exists at a large amount exceeding 0.007%, the ductility degrades. So the N content is preferably 0.007%

or less.

Cr

[0019] Chromium is an effective element for preventing softening at HAZ during welding. To attain the effect, the Cr content of 0.05% or more is necessary. If, however, the Cr content exceeds 1%, the surface property degrades. Therefore, the Cr content is specified to a range of from 0.05 to 1%.

Nb

[0020] Niobium is an effective element to prevent softening at HAZ during welding and to improve the formability by refining ferritic grains. To attain the effect, the Nb content of 0.005% or more if required. If, however, the Nb content exceeds 0.1%, the formability degrades. Therefore, the Nb content is specified to a range of from 0.005 to 0.1%.

[0021] Adding to these elements, if at least one element selected from the group consisting of 0.05 to 1% Mo, 0.02 to 0.5% V, 0.005 to 0.05% Ti, and 0.0002 to 0.002% B is added, it is more effective to further refine the ferritic grains to prevent softening at HAZ during welding and to improve the formability. In particular, Mo and V are effective to improve the hardenability, and Ti and B are effective to increase the strength.

2) Average grain size of composite structure consisting of ferrite + second phase

[0022] As described later, excellent formability is attained by making the average grain size of the composite structure 10 μm or less. The term "second phase" referred herein signifies a phase consisting of at least one structure selected from the group consisting of martensite and bainite. To the composite structure, less than 10% of pearlite or residual austenite may exist in addition to the second phase, which level thereof does not degrade the effect of the present invention.

3) Manufacturing method

[0023] The above-described high strength hot-dip galvanized steel sheet may be manufactured by a method, for example, comprising the steps of: hot-rolling a steel slab satisfying the above-given requirement of compositions at finishing temperatures of Ar3 transformation point or above; cooling the hot-rolled steel sheet within a temperature range of 800°C to 700°C at a cooling rate of 5°C/sec or more; coiling the cooled steel sheet at temperatures of 450°C to 700°C; pickling the steel sheet; and galvanizing the pickled steel sheet after heating the pickled steel sheet to a temperature range of 760°C to 880°C, and cooling the steel sheet to temperatures of 600°C or below at a cooling rate of 1°C/sec or more in a continuous hot-dip galvanizing line. The method may further comprise a step of alloying the galvanized steel sheet. The high strength hot-dip galvanized steel sheet thus manufactured is a hot-rolled steel sheet.

[0024] If the finishing temperature of the hot-rolling becomes lower than the Ar3 transformation point, coarse ferritic grains are generated to form non-uniform structure, so the finishing temperature thereof is specified to Ar3 transformation point or above.

[0025] After the hot-rolling, ferritic grains are generated in a temperature range of from 800°C to 700°C. If the cooling rate through the temperature range is less than 5°C/sec, the ferritic grains become coarse to form non-uniform structure. Consequently, the cooling is required to give at 5°C/sec or higher cooling rate. Particularly, the cooling rate between 100 and 300°C/sec is more preferable in terms of refinement of the structure.

[0026] If the coiling temperature is below 450°C, the precipitation of NbC becomes insufficient. If the coiling temperature exceeds 700°C, coarse NbC deposits to fail in refining the structure, which induces softening at HAZ during welding and degrading the formability. Consequently, the coiling temperature is specified to a range of from 450°C to 700°C.

[0027] If the heating temperature in a continuous hot-dip galvanizing line is below 760°C, the second phase cannot be formed. If the heating temperature therein exceeds 880°C, the structure becomes coarse. Therefore, the heating temperature thereof is specified to a range of from 760°C to 880°C.

[0028] After heating, even if the cooling is given at a cooling rate of less than 1°C/sec and at a cooling rate of 1°C/sec or more, when the galvanizing is given on the steel with a temperature of above 600°C, the ferritic grains become coarse or the second phase cannot be formed. Accordingly, the galvanizing is necessarily to be given after cooling the steel to 600°C or lower at a cooling rate of 1°C/sec or more.

[0029] The hot-rolled steel sheet may be subjected to galvanizing under similar condition as above in a continuous hot-dip galvanizing line after cold-rolled. The high strength hot-dip galvanized steel sheet thus manufactured is a cold-rolled steel sheet. In the procedure, the cold-rolling reduction rate of 20% or more is necessary to prevent formation of coarse structure.

[0030] Alternatively, the slab may be manufactured by ingot-making process or continuous casting process. The hot-rolling may be conducted by continuous rolling process or direct rolling process. During the hot-rolling, the steel sheet may be reheated by an induction heater. Increase in the reduction rate during the hot-rolling is preferable in terms of refinement of structure. Before applying galvanizing in a continuous hot-dip galvanizing line, Ni plating may be applied.

Example 1

[0031] Steels A through R in Table 1A which are within the range of the present invention and steels a through k in Table 1B which are outside the range of the present invention were prepared by melting in a converter, and were formed in slabs by continuous casting. The slabs were hot-rolled under the conditions of the present invention given in Table 2A, cold-rolled at a reduction rate of 60%, and then galvanized under the conditions of the present invention given in Table 2A using a continuous hot-dip galvanizing line, thus manufacturing high strength hot-dip galvanized steel sheets having 1.4 mm in thickness.

[0032] The second phase of each high strength hot-dip galvanized steel sheet was observed using an electron microscope. The residual austenite of each high strength hot-dip galvanized steel sheet was determined by an X-ray diffraction meter, and the tensile strength TS thereof was determined by a tensile test. To evaluate the characteristics at HAZ of each high strength hot-dip galvanized steel sheet after laser welding, Erichsen test was given to the mother material and to the laser-welded part to determine the formed height h0 of the mother material, the formed height ht of the welded part, and their difference Δh (= h0 - ht).

[0033] The laser welding was carried out using carbon dioxide laser (10.6 µm in wavelength, ring mode M=2 of beam mode) and ZnSe lens (254 mm of focal distance) as the convergence system, while letting Ar gas flow as the shield gas at a flow rate of 20 l/min giving 4 kW of laser output and 4 m/min of welding speed.

[0034] With the steels C, I, J, Q, and d in Table 1A and Table 1B, high strength hot-dip galvanized steel sheets were prepared under the conditions given in Table 3A. The above-described tests were applied to each of thus prepared steel sheets.

[0035] The results are given in Table 2B and Table 3B.

[0036] As for the steel sheets having the composition and the size of ferrite and of second phase within the range of the present invention, the values of Δh were small, and the HAZ softening hardly occurred. On the other hand, for the steel sheets having these characteristics outside the range of the present invention, the values of Δh were large, and rapture occurred at HAZ.

[0037] Fig. 1 shows the relation between the value of Δh and the ferritic grain size of the steel sheets given in Table 2B and Table 3B.

[0038] The grain sizes of second phase are given in Table 2B and Table 3B.

[0039] When the steels having the compositions within the range of the present invention were used, and when the manufacturing conditions within the range of the present invention were applied to make the ferritic grain size and the grain size of second phase 10 µm or less, the obtained galvanized steel sheet showed no rapture at HAZ, gave 2 mm or smaller of Δh, gave high strength, and hardly induced HAZ softening.

[0040] To the contrary, the steel sheets having the compositions outside the range of the present invention and prepared by manufacturing conditions outside the range of the present invention gave above 2 mm of Δh, induced HAZ softening, and generated rupture in HAZ.

[0041] Fig. 2A and Fig. 2B show the graphs of the hardness profile on a laser-welded cross section of the steel sheet 17 according to the present invention and the steel sheet 28 as a comparative example, respectively.

[0042] The steel sheet according to the present invention gave very little HAZ softening.

Table 1A

Steel	C	Si	Mn	P	S	sol.Al	N	Nb	Cr	Other	Remark
A	0.05	0.12	2.4	0.030	0.001	0.020	0.0025	0.015	0.10	-	Example
B	0.13	0.01	3.3	0.010	0.0006	0.031	0.0014	0.043	0.20	0.07V	Example
C	0.08	0.36	2.0	0.014	0.001	0.014	0.0023	0.020	0.06	-	Example
D	0.11	0.10	1.8	0.016	0.003	0.019	0.0025	0.026	0.85	0.05Mo	Example
E	0.05	0.02	2.8	0.023	0.007	0.020	0.0036	0.010	0.07	0.01Ti	Example
F	0.19	0.25	2.2	0.026	0.003	0.021	0.0044	0.035	0.33	-	Example
G	0.08	0.63	3.0	0.030	0.002	0.032	0.0036	0.026	0.15	0.1V	Example
H	0.10	0.25	2.5	0.006	0.004	0.012	0.0021	0.031	0.05	-	Example
I	0.06	0.23	1.9	0.032	0.002	0.024	0.0020	0.058	0.40	-	Example
J	0.07	0.25	2.3	0.025	0.0002	0.022	0.0028	0.025	0.10	0.05V	Example
K	0.10	0.15	2.7	0.026	0.002	0.023	0.0011	0.020	0.55	-	Example
L	0.08	0.25	2.0	0.032	0.002	0.018	0.0048	0.045	0.15	0.15Mo	Example
M	0.04	0.10	1.4	0.019	0.001	0.031	0.0032	0.005	0.23	0.03Ti, 0.0005B	Example
N	0.15	0.48	2.5	0.011	0.002	0.026	0.0033	0.018	0.07	-	Example
O	0.13	0.10	2.3	0.011	0.002	0.022	0.0015	0.046	0.10	-	Example
P	0.09	0.25	1.6	0.016	0.001	0.038	0.0019	0.040	0.20	-	Example
Q	0.13	0.05	2.5	0.029	0.006	0.031	0.0022	0.080	0.15	0.05Ti, 0.0003B	Example
R	0.07	0.11	2.8	0.022	0.001	0.025	0.0019	0.033	0.20	-	Example

Unit is mass%.
*: outside the range of the present invention.

Table 1B

Steel	C	Si	Mn	P	S	sol.Al	N	Nb	Cr	Other	Remark
a	0.14	0.15	1.3*	0.021	0.003	0.030	0.0016	0.035	-	-	Comparison
b	0.07	0.13	2.5	0.020	0.0006	0.036	0.0021	0.003*	0.20	-	Comparison
c	0.08	0.25	2.7	0.030	0.001	0.024	0.0022	-*	0.15	0.035Ti	Comparison
d	0.16	0.02	2.2	0.012	0.002	0.028	0.0030	-*	-*	-	Comparison
e	0.07	0.10	1.6	0.030	0.002	0.021	0.0019	0.015	-*	-	Comparison
f	0.12	0.01	3.7*	0.016	0.001	0.023	0.0026	0.015	0.10	0.05Ti, 0.0003B	Comparison
g	0.11	0.30	3.9*	0.026	0.005	0.026	0.0022	0.038	-*	-	Comparison
h	0.13	0.01	1.6	0.016	0.001	0.019	0.0026	0.055	-*	0.21Mo	Comparison
I	0.07	0.02	1.2*	0.015	0.001	0.040	0.0041	0.050	0.35	-	Comparison
j	0.09	0.25	3.7*	0.033	0.001	0.026	0.0029	-*	0.10	-	Comparison
k	0.05	0.45	2.1	0.045	0.003	0.028	0.0030	-*	-*	0.04Ti	Comparison

Unit is mass%.
*: outside the range of the present invention.

Table 2A

Steel sheet	Steel	Hot-rolling condition			Cold-rolling reduction rate %	Sheet thickness mm	Hot-dip galvanizing condition		
		Heating temp. °C	Cooling rate °C/ sec	Coiling temp. °C			Soaking temp. °C	Cooling rate °C/ sec	Alloying
1	A	1220	10	580	60	1.4	800	7	yes
2	B	1260	10	630	60	1.4	800	7	no
3	C	1230	10	600	60	1.4	800	12	yes
4	D	1170	10	530	60	1.4	800	15	yes
5	E	1220	10	620	60	1.4	800	3	yes
6	F	1200	10	600	60	1.4	800	8	yes
7	G	1200	10	580	60	1.4	800	20	yes
8	H	1200	10	580	60	1.4	800	15	no
9	I	1200	10	580	60	1.4	800	10	yes
10	J	1200	10	580	60	1.4	800	10	yes
11	K	1200	10	580	60	1.4	800	2	yes
12	L	1270	10	580	60	1.4	800	7	yes
13	M	1230	10	580	60	1.4	800	25	yes
14	N	1200	10	580	60	1.4	800	20	yes
15	O	1200	10	550	60	1.4	800	10	no
16	P	1200	10	550	60	1.4	800	10	no
17	Q	1200	10	620	60	1.4	800	5	yes
18	R	1200	10	620	60	1.4	800	7	yes
19	a	1200	10	620	60	1.4	800	5	yes
20	b	1200	10	580	60	1.4	800	28	yes
21	c	1200	10	580	60	1.4	800	10	no
22	d	1200	10	580	60	1.4	800	13	yes
23	e	1200	10	580	60	1.4	800	9	yes
24	f	1280	10	600	60	1.4	800	5	yes
25	g	1200	10	600	60	1.4	800	27	yes
26	h	1200	10	600	60	1.4	800	10	yes
27	i	1200	10	600	60	1.4	800	10	yes
28	j	1200	10	600	60	1.4	800	10	yes
29	k	1200	10	600	60	1.4	800	10	yes

Table 2B

Steel sheet	Steel	Structure					Characteristics					Remark
		Phase	Ferritic grain size µm	Second phase volumetric percentage %	Second phase grain size µm	Residual γ volumetric percentage %	TS MPa	h0 mm	ht mm	Δh mm	Position of rupture	
1	A	F+M	8	27	5	0	796	9.4	9.1	0.3	Weld line	Example
2	B	F+M	5	67	3	3	1152	6.9	6.8	0.1	Weld line	Example
3	C	F+M+B	9	23	7	0	739	9.8	9.2	0.6	Weld line	Example
4	D	F+M	7	32	5	1	889	8.8	8.8	0	Weld line	Example
5	E	F+M	10	38	8	1	861	9.0	8.0	1.0	Weld line	Example
6	F	F+M+B	6	55	4	6	1045	7.7	7.2	0.5	Weld line	Example
7	G	F+M	8	62	5	2	1097	7.3	7.3	0	Weld line	Example
8	H	F+M+B	3	50	7	3	860	9.0	9.0	0	Weld line	Example
9	I	F+M	2	41	6	0	842	9.1	9.1	0	Weld line	Example
10	J	F+M	4	46	5	1	815	9.3	9.1	0.2	Weld line	Example
11	K	F+M	7	65	9	1	1079	7.5	7.3	0.2	Weld line	Example
12	L	F+M+B	5	33	5	0	815	9.3	9.3	0	Weld line	Example
13	M	F+M+B	10	28	8	0	764	9.7	8.5	1.2	Weld line	Example
14	N	F+M	8	46	4	3	959	8.3	7.7	0.6	Weld line	Example
15	O	F+M+B	5	31	7	2	847	9.1	9.1	0	Weld line	Example
16	P	F+M	3	25	10	0	719	10.0	9.9	0.1	Weld line	Example
17	Q	F+M	3	55	3	4	1071	7.5	7.3	0.2	Weld line	Example
18	R	F+M	6	43	5	1	977	8.2	8.1	0.1	Weld line	Example
19	a	F+P	8	-	-	0	552	11.1	8.6	2.5	HAZ	Comparison
20	b	F+M	12	39	15	1	905	8.7	4.9	3.8	HAZ	Comparison
21	c	F+M	15	46	13	1	953	8.3	2.0	6.3	HAZ	Comparison

Table 2B (continued)

Steel sheet	Steel	Structure					Characteristics					Remark
		Phase	Ferritic grain size µm	Second phase volumetric percentage %	Second phase grain size µm	Residual γ volumetric percentage %	TS MPa	h0 mm	ht mm	Δh mm	Position of rupture	
22	d	F+M+B	13	23	20	1	777	9.6	4.4	5.2	HAZ	Comparison
23	e	F+M	8	7	9	0	549	11.2	7.2	4.0	HAZ	Comparison
24	f	F+M	5	83	16	3	1323	5.7	1.4	4.3	HAZ	Comparison
25	g	F+M	3	65	25	5	1196	6.6	4.3	2.3	HAZ	Comparison
26	h	F+M+B	7	16	8	0	647	10.5	5.9	4.6	HAZ	Comparison
27	I	F+P	13	-	-	0	640	10.5	6.3	4.2	HAZ	Comparison
28	j	F+M	10	70	30	2	1181	6.7	3.2	3.5	HAZ	Comparison
29	k	F+M+B	16	20	13	1	710	10.0	3.1	6.9	HAZ	Comparison

F: ferrite, M: martensite, B: bainite, P: pearlite

Table 3A

Steel sheet	Steel	Hot-rolling condition			Cold-rolling reduction rate %	Sheet thickness mm	Hot-dip galvanizing condition		
		Heating temp. °C	Cooling rate °C/ sec	Coiling temp. °C			Soaking temp. °C	Cooling rate °C/ sec	Alloying
41	C	1240	1	550	60	1.4	780	5	yes
42	C	1240	3	550	60	1.4	780	5	yes
43	C	1240	8	550	60	1.4	780	5	yes
44	C	1240	15	550	60	1.4	780	5	yes
45	C	1240	100	550	60	1.4	780	5	yes
46	C	1240	15	550	-	3.5	780	5	no
47	C	1240	15	550	10	3.15	780	5	no
48	C	1240	15	550	30	2.45	780	5	no
49	C	1240	15	550	80	0.7	780	5	no
50	I	1200	15	620	-	2.3	780	5	yes
51	J	1250	15	580	60	1.4	700	8	yes
52	J	1250	15	580	60	1.4	750	8	yes
53	J	1250	15	580	60	1.4	780	8	yes
54	J	1250	15	580	60	1.4	830	8	yes
55	J	1250	15	580	60	1.4	860	8	yes
56	J	1250	15	580	60	1.4	900	8	yes
57	J	1250	15	580	60	1.4	800	0.5	yes
58	J	1250	15	580	-	2.3	800	8	yes
59	Q	1200	10	400	60	1.4	780	5	yes
60	Q	1200	200	500	60	1.4	780	5	yes
61	Q	1200	10	680	60	1.4	780	5	yes
62	Q	1200	10	600	-	3.5	780	5	yes
63	d	1250	15	580	60	1.4	900	8	yes
64	d	1250	15	580	10	3.15	800	8	yes

Table 3B

Steel sheet	Steel	Structure					Characteristics					Remark
		Phase	Ferritic grain size μm	Second phase volumetric percentage %	Second phase grain size μm	Residual γ volumetric percentage %	TS MPa	h0 mm	ht mm	Δh mm	Position of rupture	
41	C	F+M+B	15	25	12	0	730	9.0	2.3	6.7	HAZ	Comparison
42	C	F+M+B	13	23	10	0	725	9.2	3.5	5.7	HAZ	Comparison
43	C	F+M+B	9	25	8	0	720	10.1	9.3	0.8	Weld line	Example
44	C	F+M+B	7	24	7	0	733	9.8	9.3	0.5	Weld line	Example
45	C	F+M+B	3	27	5	0	735	10.3	10.3	0	Weld line	Example
46	C	F+M+B	7	25	8	0	720	11.5	11.3	0.2	Weld line	Example
47	C	F+M+B	20	22	13	0	715	8.9	1.1	7.8	HAZ	Comparison
48	C	F+M+B	8	26	10	0	726	10.8	10.0	0.8	Weld line	Example
49	C	F+M+B	3	25	5	0	725	9.5	9.5	0	Weld line	Example
50	I	F+M	5	38	6	0	820	9.2	9.2	0	Weld line	Example
51	J	F+P	11	-	-	0	1121	4.2	1.5	2.7	HAZ	Comparison
52	J	F+P	11	-	-	0	965	6.3	3.9	2.4	HAZ	Comparison
53	J	F+M	5	45	7	1	820	9.5	9.5	0	Weld line	Example
54	J	F+M	6	48	6	1	808	9.8	9.8	0	Weld line	Example
55	J	F+M	4	46	5	1	806	9.7	9.7	0	Weld line	Example
56	J	F+M	15	45	14	0	795	9.1	3.6	5.5	HAZ	Comparison
57	J	F+P	7	-	-	0	700	9.3	6.8	2.5	HAZ	Comparison
58	J	F+M	5	43	5	1	817	10.7	10.7	0	Weld line	Example
59	Q	F+M	12	50	8	3	1050	7.3	3.1	4.2	HAZ	Comparison
60	Q	F+M	2	53	3	4	1061	7.6	7.5	0.1	Weld line	Example
61	O	F+M	4	48	6	4	1058	7.7	7.7	0	Weld line	Example

Table 3B (continued)

Steel sheet	Steel	Structure					Characteristics					Remark
		Phase	Ferritic grain size µm	Second phase volumetric percentage %	Second phase grain size µm	Residual γ volumetric percentage %	TS MPa	h0 mm	ht mm	Δh mm	Position of rupture	
62	Q	F+M	7	51	5	3	1055	9.0	9.0	0	Weld line	Example
63	d	F+M+B	18	25	15	1	765	9.5	1.9	7.6	HAZ	Comparison
64	d	F+M+B	25	22	23	1	749	9.3	2.1	7.2	HAZ	Comparison

F: ferrite, M: martensite, B: bainite, P: pearlite

Claims

1. A high strength hot-dip galvanized steel sheet consisting essentially of 0.03 to 0.25% C, 0.7% or less Si, 1.4 to 3.5% Mn, 0.05% or less P, 0.01% or less S, 0.05 to 1% Cr, 0.005 to 0.1% Nb, by mass, and balance of Fe, and being made of a composite structure of ferrite and secondary phase, the average grain size of the composite structure being 10 μm or smaller.

2. The high strength hot-dip galvanized steel sheet of claim 1 further containing at least one element selected from the group consisting of 0.05 to 1% Mo, 0.02 to 0.5% V, 0.005 to 0.05% Ti, and 0.0002 to 0.002% B, by mass.

3. A method for manufacturing high strength hot-dip galvanized steel sheet comprising the steps of:

hot-rolling a steel slab consisting essentially of 0.03 to 0.25% C, 0.7% or less Si, 1.4 to 3.5% Mn, 0.05% or less P, 0.01% or less S, 0.05 to 1% Cr, 0.005 to 0.1% Nb, by mass, and balance of Fe, at temperatures of Ar3 transformation point or above;
cooling the hot-rolled steel sheet within a temperature range of 800°C to 700°C at a cooling rate of 5°C/sec or more, followed by coiling the cooled steel sheet at temperatures of 450°C to 700°C;
pickling the steel sheet; and
galvanizing the pickled steel sheet after heating the pickled steel sheet to a temperature range of 760°C to 880°C, and cooling the steel sheet to temperatures of 600°C or below at a cooling rate of 1°C/sec or more in a continuous hot-dip galvanizing line.

4. A method for manufacturing high strength hot-dip galvanized steel sheet comprising the steps of:

hot-rolling a steel slab consisting essentially of 0.03 to 0.25% C, 0.7% or less Si, 1.4 to 3.5% Mn, 0.05% or less P, 0.01% or less S, 0.05 to 1% Cr, 0.005 to 0.1% Nb, further containing at least one element selected from the group consisting of 0.05 to 1% Mo, 0.02 to 0.5% V, 0.005 to 0.05% Ti, and 0.0002 to 0.002% B, by mass, and balance of Fe, at temperatures of Ar3 transformation point or above;
cooling the hot-rolled steel sheet within a temperature range of 800°C to 700°C at a cooling rate of 5°C/sec or more, followed by coiling the cooled steel sheet at temperatures of 450°C to 700°C;
pickling the steel sheet; and
galvanizing the pickled steel sheet after heating the pickled steel sheet to a temperature range of 760°C to 880°C, and cooling the steel sheet to temperatures of 600°C or below at a cooling rate of 1°C/sec or more in a continuous hot-dip galvanizing line.

5. The method for manufacturing high strength hot-dip galvanized steel sheet of claim 3 further comprising the step of cold-rolling the steel sheet at a reduction rate of 20% or higher between the step of pickling and the step of galvanizing.

6. The method for manufacturing high strength hot-dip galvanized steel sheet of claim 4 further comprising the step of cold-rolling the steel sheet at a reduction rate of 20% or higher between the step of pickling and the step of galvanizing.

7. The method for manufacturing high strength hot-dip galvanized steel sheet of claim 3 further comprising the step of alloying the galvanized steel sheet after the step of galvanizing.

8. The method for manufacturing high strength hot-dip galvanized steel sheet of claim 4 further comprising the step of alloying the galvanized steel sheet after the step of galvanizing.

9. The method for manufacturing high strength hot-dip galvanized steel sheet of claim 5 further comprising the step of alloying the galvanized steel sheet after the step of galvanizing.

10. The method for manufacturing high strength hot-dip galvanized steel sheet of claim 6 further comprising the step of alloying the galvanized steel sheet after the step of galvanizing.

FIG. 1

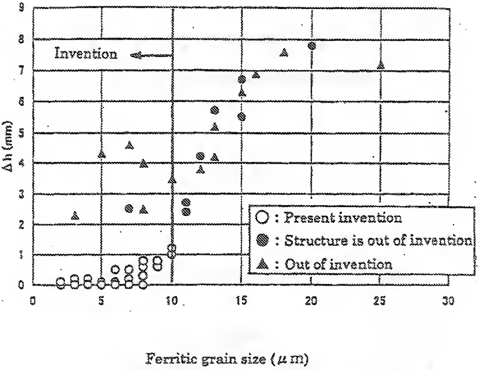

Δh (mm)
Invention
○ : Present invention
● : Structure is out of invention
▲ : Out of invention
Ferritic grain size (μm)

FIG. 2A

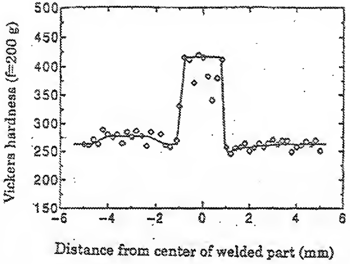
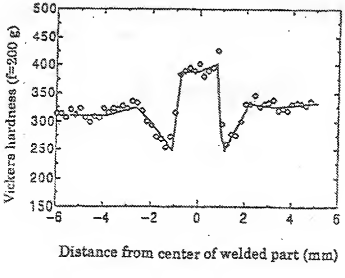

Vickers hardness (f=200 g)
500
450
400
350
300
250
200
150
-6
-4
-2
0
2
4
6
Distance from center of welded part (mm)

FIG. 2B


Vickers hardness (f=200 g)
500
450
400
350
300
250
200
150
-6
-4
-2
0
2
4
6
Distance from center of welded part (mm)

INTERNATIONAL SEARCH REPORT

International application No.
PCT/JP02/01711

A. CLASSIFICATION OF SUBJECT MATTER
Int.Cl⁷ C22C38/00, C21D9/46

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
Int.Cl⁷ C22C38/00-60, C21D9/46-48, 8/00-04

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched
Jitsuyo Shinan Koho 1926-1996 Toroku Jitsuyo Shinan Koho 1994-2002
Kokai Jitsuyo Shinan Koho 1971-2002 Jitsuyo Shinan Toroku Koho 1996-2002

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)
WPI

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	JP 11-343538 A (Kawasaki Steel Corp.), 14 December, 1999 (14.12.99), Claims (Family: none)	1-10
X	JP 2000-282175 A (Kawasaki Steel Corp.), 10 October, 2000 (10.10.00), Claims (Family: none)	2
X	JP 2000-109951 A (Kawasaki Steel Corp.), 18 April, 2000 (18.04.00), Claims (Family: none)	2

[X] Further documents are listed in the continuation of Box C. [ ] See patent family annex.

* Special categories of cited documents:
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"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
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"&" document member of the same patent family

Date of the actual completion of the international search	Date of mailing of the international search report
21 May, 2002 (21.05.02)	04 June, 2002 (04.06.02)
Name and mailing address of the ISA/ Japanese Patent Office	Authorized officer
Facsimile No.	Telephone No.

INTERNATIONAL SEARCH REPORT

International application No.
PCT/JP02/01711

C (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
E,X	EP 1143022 A1 (NKK Corp.), 10 October, 2001 (10.10.01), & US 2002/0000256 A1 & KR 2001075195 A & JP 2001-152255 A & JP 2002-30347 A & WO 01/20051 A1	1-10
A	JP 11-236621 A (Sumitomo Metal Industries, Ltd.), 31 August, 1999 (31.08.99), (Family: none)	1-10

Form PCT/ISA/210 (continuation of second sheet) (July 1998)